



and guaranteeing Y/T values in compliance with the European market requirements.

The approach used to achieve this goal and the results obtained after the first year of operation are the subject of this article.

**METALLURGICAL DESIGN APPROACH**

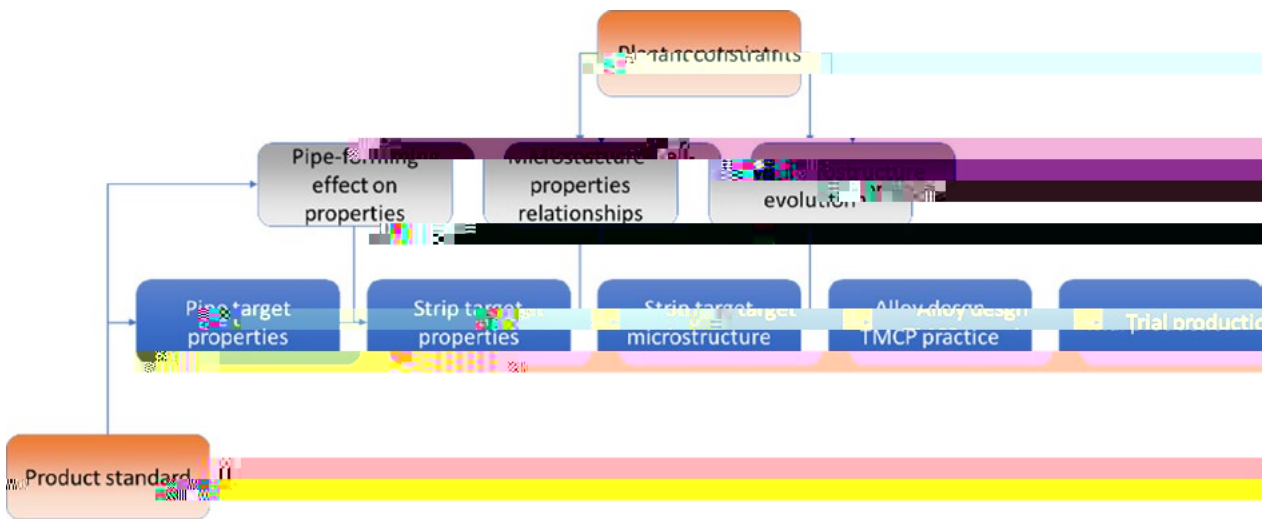
The typical CSM approach to the metallurgical design of structural steels, schematically described in the Fig.1, was used, and followed in its general lines.

In summary, this approach consists of four successive steps:

- Definition of the target properties on strip from the

specified properties on pipe and knowledge of the effect that the pipe forming processes has on the properties:

- Definition of target microstructure from the target properties identified in the previous step and knowledge of the relationship between microstructure and steel properties;
- Definition (or verification) of the rolling and cooling operating practices to be applied to the steel to obtain the microstructure and properties identified in the previous steps;
- Verification by industrial testing of the accuracy of the settings and definition of possible corrective actions.



**Fig.1** - Typical CSM approach to the metallurgical design of structural steels.

**Definition of the strip target properties**

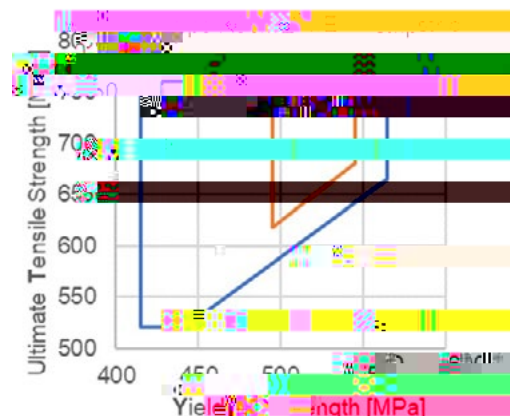
The target properties of the pipe, taken from the standard, are summarised in the Tab.1 and Fig.2.

Fig.2 also shows the restriction of the target property win-

dow of the strip necessary to account for the loss of mechanical properties when forming the pipe and to compensate the variability due to rolling.

**Tab.1** - Target properties of pipe and strip.

| TARGET PROPERTIES |      |           |           |
|-------------------|------|-----------|-----------|
| Property          | Unit | Pipe      | Strip     |
| Y                 | MPa  | 415 ÷ 565 | 495 ÷ 545 |
| T                 | MPa  | 520 ÷ 760 | 590 ÷ 730 |
| Y/T               | -    | 0.85      | 0.80      |



**Fig.2** - Target properties windows of pipe and strip.

The effect of grain size on mechanical properties consists in the fact that yield strength and ultimate tensile strength values remain constant with impact toughness values a dispersion of yield strength values with grain size ratio were not observed. The data into account are summarised in Table 1. Subsequent

$$Y_{FP} = Y_0 + \frac{k_Y}{\sqrt{d}} \quad ; \quad T_{FP} = T_0 + \frac{k_T}{\sqrt{d}}$$

where  $Y_0$  and  $T_0$  are the tensile strength and impact toughness size characteristic values,  $k_Y$  and  $k_T$  are the coefficients of the equations. The values of  $k_Y$  and  $k_T$  are known terms

$$Y_{FP} = 62.6 + 26.1[Mn] + 60.2[Si] + 759[P] + 80[Cu] + 60[Cr] + 45[Ni] + 11[Mo] + 19.7 \sqrt{\frac{1000}{d}} + 2000[Nb] + 1000[V]$$

Based on the results of the tests with 0.1 and 0.05 mm grain sizes, the grain size required to obtain a ferrite-pearlite structure

$$\frac{Y_{FP}}{T_{FP}} = \frac{Y_{FP} \cdot (PF\%) + Y_{FP} \cdot (B\%) + Y_{FP} \cdot (MA\%)}{T_{FP} \cdot (PF\%) + T_{FP} \cdot (B\%) + T_{FP} \cdot (MA\%)}$$

where (PF%) is the percentage of polygonal ferrite, (B%) is the percentage of bainite while the coefficient

Fig.3 (a) shows the results obtained by applying equations (4) – (6) to the steel grade LC1, used in the past to produce ERW X65ME pipes; in particular, the optimal micro-

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## CONCLUSIONS

Acciaierie d'Italia and Rina Consulting Centro Sviluppo Materiali are collaborating on the development of natural gas and hydrogen transport steels. CSM's typical approach for metallurgical design of pipe steels was adapted to the case of interest and used to define chemical composition and operating practices that allow to manufacture ERW pipes of grade X60ME, without exceeding 0.12% of the carbon.

Concerning to it, the results of the industrial test are sati-

sfying for the validation of methodology and the pipes are in compliance with the ISO3183. However, in the future it might be interesting to further investigate the system to:

- reduce material yield strength, which is considered high even if in line with standard requirements;
- keep, or improve, Y/T values;
- contain the mechanical properties dispersion to avoid the risk of non-conformity;
- and test the material in hydrogen atmosphere.

## REFERENCES

- [1] ISO 3183:2019 p. 8;
- [2] Hodgson Gibbs, ISIJ Int. 32-12, 1329-1338;
- [3] European Commission, Directorate-General for Research and Innovation, Gutiérrez, I., Parker, S., Wadsworth, J., Property models for mixed microstructures: final report, Publications Office, 2003;
- [4] Pokutyłowicz, Collins, Baragar, Yue: Properties-Prediction Model for the Hot Rolling of Long Products, 37th MWSP Conf. Proc., ISS, 1996, Vol. 33, pp427-431.

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