pred

opment of a model for the of mechanical properties for AI-Si-Mg castings

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A356 alloy is v Generally, a T casting. Nowa designing sou are not given. additional pre as-cast prope mechanical pr thicknesses ar carried out. Su used to verify t provided by sim after T6 heat treat structural components by means of Low Pressure Die Casting (LPDC) process. on, quenching and aging treatment) is carried out to improve the strength of the n of casting processes and solidification phenomena is a common practice for rechanical strength values and their correlation with microstructure parameters o predict material behaviour before producing the castings would represent an naterial properties. In the present study, a model for the estimation of tensile llation was validated on a 22" wheel obtained by LPDC. Microstructural and on the component both in as-cast and T6 condition. First, areas with different analysed and secondary dendrite arm spacing (SDAS) measurements were te performed on specimens from rim and spokes. Experimental data were sults and to validate the as-cast model. Based on additional information pental data, a mathematical model to predict the mechanical properties

KEYWORDS: ALUMINUM, HEAT TREATMENT, SIMULATION, MODEL, CASTING;

NTRODUCTION

A356 is an aluminum casting alloy wide of its good castability, corrosion resistance and r cal properties, in particular high strength-to-weight ratio, which make it suitable for various applications in the automotive industry [1]. In order to allow its use in structural application, generally a T6 heat treatment is carried out to further increase the strength of the castings [2]. Nowadays the quality of castings is constantly improving, also thanks to casting simulation software that provide results in terms of microstructure, defects like shrinkage porosity, solidification time, fraction solid and residual stresses [3] by modelling both mold filling and solidification phenomena. For instance, Sadeghi et al. [4] used simulation to predict fluid flow and solidification steps of the castings while Aloe et al. [5] focused their attention on the development of numerical tools to successfully predict stresses, microstructures and defects. Commercial casting software are not able to provide mechanical

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strength values before and after heat treatment. However, the possibility to predict the material behavior would represent a precious tool for exploiting material properties and simplifying production processes.

The aim of the work is to develop a mathematical model to successfully predict the local mechanical strength of the casting from the main microstructural parameters. In particular, specific equations to predict yield strength and ultimate tensile strength for the as-cast and T6 conditions were studied using the commercial software ProCAST®. First, microstructural and mechanical properties were investigated on a 22" wheel obtained by LPDC process both in as-cast and T6 conditions. In parallel, using casting and geometrical parameters given by the foundry, a complete simulation was set up and a predictive model for as-cast condition was developed by exploiting the results. Experimental data were used for two main reasons; first, microstructural properties were used to verify the reliability of results from the casting simulation and then the validation of the predictive models for as-cast condition was carried out based on experimental tensile properties. Finally, a T6 model was proposed by extending the as-cast model previously validated.

EXPERIMENTAL PROCEDURE

The experimental tests were performed on two 22" wheels obtained by LPDC using A356 alloy, one in as-cast condition, the other one after T6 treatment. The T6 heat treatment performed by the foundry consisted of solution treatment at 530 °C, quenching and then aging at 146 °C for 3 hours. A preliminary analysis was carried out in different positions of the as-cast wheel in order to analyze the influence of geometry and cooling rate on microstructure and to identify relevant sections for further characterization.

Five samples from the main spoke (letter A) and three from the minor one (letter B) were taken from the as-cast component in order to investigate different thicknesses:

A1 and B1 from the rim, A2 at the root of the spoke, A3, A4,

B3, B4 from the spokes and A5 close to the hub (Fig. 1).

Fiewer samples were examined on the second spoke be
Dates a ratter - a ppet 18 min hardy. Startypist on the main one, it was

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Tab.2 - Validation of as cast model.

YS f 🐪 he 🚣 'de [MPa]	E je i e a YS[MPa]
86.9	87.7 ± 2.1
94.8	92.8 ± 1.9
94.6	96 ± 1.4

A model for the developed, but as cast model

extension of the tensile tests. The following equation is proposed:



ULTIMATE TENS

After a study of lite. udwig model represents the most reliable equation to predict UTS:

$$UTS = YS + K * \varepsilon^{\alpha}$$

where K is a function of SDAs parameters. However, also casting a poro-

Tab.3 - Validation of as cast model.

	UTS f 🗯 he 🗸 'de [MPa]	E	re i e a UTS	[MPa]
A1	159.2		160.4 ± 7.3	
A3	168.1		163.6 ± 6.1	
В3	163.3		165.5 ± 5.9	

CONCLUSIONS

In this study, a mathematical model to predict tensile behavior of A356 both for as-cast and T6 conditions as a function of microstructural parameters is proposed.

First, the yield strength was found to depend on SDAS and experimental values ensured the validation of the model for the as-cast condition. The same model was extended to predict the material behavior after heat treatment and new coefficients were found.

The ultimate tensile strength of the alloy was found to depend on SDAS, defects content and tensile parameters.

After the validation of this model for the as-cast condi-

tions, a new predictive equation was developed also for T6 conditions by exploiting experimental values. The two equations result to be the same since the difference lies in the value of each variable involved.

The good results obtained suggest that the proposed models could be integrated in the casting simulation software to obtain the local distribution of mechanical properties to be used during the re-design step of a new component. In this way, a reduction of thicknesses, where possible, can be achieved, and the always more restricted criteria for the lightening of vehicles can be thet.

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